

GEOTECHNICAL AND GEOLOGIC HAZARDS INVESTIGATION 2294 TALL GRASS DRIVE GRAND JUNCTION, COLORADO PROJECT #01282-0002

FOOD BANK OF THE ROCKIES 10700 E. 45 AVENUE DENVER, COLORADO 80239

MARCH 31, 2021

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SUMMARY OF CONCLUSIONS AND RECOMMENDATIONS

A geologic hazards and geotechnical investigation was conducted at 2294 Tall Grass Drive in Grand Junction, Colorado. The project location is shown on Figure 1 – Site Location Map. The purpose of the investigation was to evaluate the surface and subsurface conditions at the site with respect to geologic hazards, foundation design, pavement design, and earthwork for the proposed construction. This summary has been prepared to include the information required by civil engineers, structural engineers, and contractors involved in the project.

Subsurface Conditions (p. 2)

The subsurface investigation consisted of seven borings, drilled on March 10^{th} , 2021. The locations of the borings are shown on Figure 2 – Site Plan. The borings generally encountered native clay soils over dense sandy gravel soils. Groundwater was encountered in the borings at depths ranging from 7.0 to 13.0 feet the time of the investigation. The native clay soils were indicated to be moderately plastic and are anticipated to be slightly to moderately expansive.

Geologic Hazards and Constraints (p. 3)

The primary geologic hazard at the site is the presence of moisture sensitive soils. However, shallow groundwater may also impact the construction.

Summary of Foundation Recommendations

Spread Footings

- Structural Fill Minimum of 36-inches below foundations. Imported structural fill should consist of granular material approved by HBET.(p. 4)
- Maximum Allowable Bearing Capacity 1,500 psf. (p. 4)
- Subgrade Modulus 150 pci for native soils. 200 pci for approved imported materials. (p. 4)

Waffle Slab

- *Maximum Allowable Bearing Capacity* 1,500 psf. (p. 4)
- Subgrade Modulus 150 pci for native soils. 200 pci for approved imported materials. (p. 4)

Helical Piles

- Anticipated Length 20 to 35 feet. (p. 5)
- Anticipated Capacity 40 to 60 tons based upon load testing. (p. 5)

Summary of Pavement Recommendations (p. 6)

Automobile Parking Areas

EDLA = 5, Structural Number = 2.75

	PAVEMENT SECTION (Inches)									
ALTERNATIVE	Hot-Mix Asphalt Pavement	CDOT Class 6 Base Course	CDOT Class 3 Subbase Course	Concrete Pavement	TOTAL					
А	3.0	10.0			13.0					
В	4.0	7.0			11.0					
С	3.0	6.0	6.0		15.0					
Rigid Pavement		6.0		6.0	12.0					

Truck Traffic Areas

EDLA = 20, Structural Number = 3.50

	PAVEMENT SECTION (Inches)									
ALTERNATIVE	Hot-Mix Asphalt Pavement	CDOT Class 6 Base Course	CDOT Class 3 Subbase Course	Concrete Pavement	TOTAL					
А	3.0	15.0			18.0					
В	4.0	12.0			16.0					
С	3.0	6.0	13.0		22.0					
Rigid Pavement		6.0		8.0	14.0					

TABLE OF CONTENTS

1.0	INTRODUCTION	1
1.1	Scope	1
1.2	Site Location and Description	1
1.3	Proposed Construction	1
2.0	GEOLOGIC SETTING	2
2.1	Soils	2
2.2	Geology	2
2.3	Groundwater	2
3.0	FIELD INVESTIGATION	2
3.1	Subsurface Investigation	2
3.2	Field Reconnaissance	
4.0	LABORATORY TESTING	3
5.0	GEOLOGIC INTERPRETATION	3
5.1	Geologic Hazards	
5.2	Geologic Constraints	3
5.3	Water Resources	3
5.4	Mineral Resources	4
6.0	CONCLUSIONS	4
7.0	RECOMMENDATIONS	
7.1	Foundations	
7.2	Corrosion of Concrete and Steel	6
7.3	Non-Structural Floor Slabs and Exterior Flatwork	7
7.4	Lateral Earth Pressures	7
7.5	Drainage	7
7.6	Excavations	
7.7	Pavements	8
8.0	GENERAL	9

FIGURES

Figure 1 – Site Location Map Figure 2 – Site Plan

APPENDICES

Appendix A – UDSA NRCS Soil Survey Data Appendix B – Typed Boring Logs Appendix C – Laboratory Testing Results



1.0 INTRODUCTION

As part of extensive development in Western Colorado, new construction is proposed at 2294 Tall Grass Drive in Grand Junction. As part of the development process, Huddleston-Berry Engineering and Testing, LLC (HBET) was retained by Food Bank of the Rockies to conduct a geologic hazards and geotechnical investigation at the site.

1.1 Scope

As discussed above, a geologic hazards and geotechnical investigation was conducted for 2294 Tall Grass Drive in Grand Junction, Colorado. The scope of the investigation included the following components:

- Conducting a subsurface investigation to evaluate the subsurface conditions at the site.
- Collecting soil samples and conducting laboratory testing to determine the engineering properties of the soils at the site.
- Providing recommendations for foundation type and subgrade preparation.
- Providing recommendations for bearing capacity.
- Providing recommendations for lateral earth pressure.
- Providing recommendations for drainage, grading, and general earthwork.
- Providing recommendations for pavements.
- Evaluating potential geologic hazards at the site.

The investigation and report were completed by a Colorado registered professional engineer in accordance with generally accepted geotechnical and geological engineering practices. This report has been prepared for the exclusive use of Food Bank of the Rockies.

1.2 Site Location and Description

The site is located at 2294 Tall Grass Drive in Grand Junction, Colorado. The project location is shown on Figure 1 – Site Location Map.

At the time of the investigation, the site was generally open with a general slope down towards the south. Vegetation at the site consisted primarily of grasses and weeds. The site was bordered to the north by G Road, to the south by Tall Grass Drive, to the west by Long Acres Drive, and to the east by 23 Road.

1.3 Proposed Construction

The proposed construction is anticipated to include a new commercial structure, utility installation, and pavements. The proposed structure may be wood framed, steel framed, or masonry.



2.0 GEOLOGIC SETTING

2.1 Soils

Soils data was obtained from the USDA Natural Resource Conservation Service Web Soil Survey. The data indicates that the soils at the site consist of Massadona silty clay loam, saline surface, 0 to 2 percent slopes. Soil survey data, including a description of the soil unit, is included in Appendix A.

Structure construction in the site soils is described as being somewhat limited due to shrink-swell. Road construction in the Massadona soils is described as being very limited due to low strength and/or shrink-swell. Excavation in the site soils is described as being somewhat limited due to dust, clay content, and/or unstable excavation walls. The site soils are indicated to have a low potential for frost action, high risk of corrosion of uncoated steel, and high risk of corrosion of concrete.

2.2 Geology

According to the *Geologic Map of Colorado National Monument and Adjacent Areas, Mesa County, Colorado* (2001), the site is underlain by sheetwash deposits.

2.3 Groundwater

Groundwater was encountered at depths ranging from 7.0 to 13.0 feet in the subsurface at the time of the investigation.

3.0 FIELD INVESTIGATION

3.1 Subsurface Investigation

The subsurface investigation was conducted on March 10^{th} , 2021 and consisted of seven borings as shown on Figure 2 – Site Plan. The borings were drilled to depths ranging from 11.5 to 21.0 feet below the existing ground surface. Typed boring logs are included in Appendix B. Samples of the native soils were collected during Standard Penetration Testing (SPT) at the locations shown on the logs.

As indicated on the logs, the subsurface conditions at the site were slightly variable. Borings B-1, B-5, and B-7, conducted in the northeast and western portions of the site, encountered 1.0 foot of topsoil above brown to gray to reddish-brown, moist to wet, soft to very stiff lean clay soils to the bottoms of the borings. Groundwater was encountered in B-1 and B-5 at respective depths of 13.0 and 9.0 feet at the time of the investigation.



Borings B-2, B-3, B-4, and B-6 were conducted in the southeast and center portions of the site. The borings encountered 1.0 foot of topsoil above brown, moist to wet, soft to hard, lean clay soils to depths ranging from 17.0 to 19.5 feet. The lean clay soils were underlain by brown, wet, dense to very dense sandy gravels to the bottoms of the borings. Groundwater was encountered in the borings at depths ranging from 7.0 to 10.0 feet at the time of the investigation.

3.2 Field Reconnaissance

The field reconnaissance included walking the site during the subsurface investigation. In general, the site was fairly level and no evidence of active landslides, debris flows, rockfalls, etc. was observed.

4.0 LABORATORY TESTING

Selected native soil samples collected from the borings were tested in the Huddleston-Berry Engineering and Testing LLC geotechnical laboratory for natural moisture content determination, grain size analysis, and Atterberg limits determination. The laboratory testing results are included in Appendix C.

The laboratory testing results indicate that the native clay soils are moderately plastic. In general, based upon the Atterberg limits and upon experience with similar soils in the vicinity of the subject site, the native clay soils are anticipated to be slightly to moderately expansive.

5.0 GEOLOGIC INTERPRETATION

5.1 Geologic Hazards

The primary geologic hazard at the site is the presence of moisture sensitive soils.

5.2 Geologic Constraints

The primary geologic constraint to construction at the site is the presence of moisture sensitive soils. However, shallow groundwater may impact deep utility installation at the site.

5.3 Water Resources

No water supply wells were observed on the property. However, shallow groundwater was encountered at the site. In general, with proper design and construction, development of the site is not anticipated to adversely affect surface water or groundwater.



5.4 Mineral Resources

Potential mineral resources in Western Colorado generally include sand, gravel, uranium ore, and commercial rock products such as flagstone. As discussed previously, gravels, cobbles, and boulders were encountered across the site. However, the gravels were deep. As a result, HBET does not believe that the gravels at the site represent an economically recoverable resource.

6.0 CONCLUSIONS

Based upon the available data sources, field investigation, and nature of the proposed construction, HBET does not believe that there are any geologic conditions which should preclude construction at the site. However, the presence of moisture sensitive soils and shallow groundwater may impact the design and construction.

7.0 **RECOMMENDATIONS**

7.1 Foundations

Based upon the results of the subsurface investigation, both shallow and deep foundations are appropriate. Where structural loads are small, shallow foundations may be acceptable. However, where significant foundation loads are anticipated, deep foundations may be preferable. The alternatives are discussed in the following sections.

Spread Footings

. Spread footings are appropriate for support of the structure; however, as discussed above, the native clay soils are anticipated to be slightly to moderately expansive. Therefore, in order to provide a uniform bearing stratum and reduce the risk of excessive differential movements, it is recommended that the foundations be constructed above a minimum of 36-inches of structural fill.

Due to their plasticity, the native soils are not suitable for reuse as structural fill. Imported structural fill should consist of a granular, non-expansive, <u>non-free draining</u> material approved by HBET.

Prior to placement of structural fill, it is recommended that the bottom of the foundation excavation be scarified to a depth of 6 to 8 inches, moisture conditioned, and compacted to a minimum of 95% of the standard Proctor maximum dry density, within \pm 2% of the optimum moisture content as determined in accordance with ASTM D698. Structural fill should extend laterally beyond the edges of the foundations a distance equal to the thickness of structural fill. Structural fill should be moisture conditioned, placed in maximum 8-inch loose lifts, and compacted to a minimum of 95% of the standard Proctor maximum dry density for fine grained soils and 90% of the modified Proctor maximum dry density for coarse grained soils, within \pm 2% of the optimum



moisture content as determined in accordance with ASTM D698 and D1557, respectively.

Structural fill should be extended to within 0.1-feet of the bottom of the foundation. No more than 0.1-feet of gravel should be placed below the footings or turndown edge as a leveling course.

For structural fill consisting of imported granular materials, and foundation building pad preparation as recommended, a maximum allowable bearing capacity of 1,500 psf may be used. In addition, a modulus of 200 pci may be used for structural fill consisting of approved materials. Foundations subject to frost should be at least 24 inches below the finished grade.

Ribbed or Waffle Structural Slab

Whereas spread footing type foundations above expansive subgrades are intended to reduce the potential for movement by spreading expansion pressures through the structural fill, structural waffle slab foundations are anticipated to move. However, this type of foundation should be designed such that the entire slab and structure move together under isolated expansive pressures. Slab bending is typically limited by the use of several grade beams or 'ribs' at the base of the slab to provide rigidity. The depth, thickness, and location of the ribs should be determined by the structural engineer.

In general, it is recommended that the grade beams below the slab be excavated into the native soils or into a layer of structural fill. Subgrade preparation, structural fill materials, and structural fill placement should be in accordance with the *Spread Footings* section of this report.

For the foundation building pad prepared as recommended with grade beams extending into the native clay soils or into structural fill, a maximum allowable bearing capacity of 1,500 psf may be used. In addition, a modulus of subgrade reaction of 200 pci may be used for structural fill consisting of approved materials. Foundations subject to frost should be at least 24 inches below the finished grade.

Helical Piles

Helical piles consist of circular or square steel shafts with load carrying helices attached to them. Some of these types of piers are proprietary. In general, the precise type, size, and quantity of piles should be established by the contractor in conjunction with the structural engineer. However, HBET provides the following design comments.

In general, helical piles should be designed to penetrate the upper clay soils and bear into the dense gravel and cobble soils. To eliminate reductions in capacity from group effects, the piles should be spaced a distance equal to three times the diameter of the largest helix. It is anticipated that the helical piles will reach refusal within 3 to 15 feet of the top of the gravel and cobble soils. Therefore, pile lengths of up to approximately 35 feet may be possible.



Based upon our experience with other projects utilizing helical piles, allowable axial capacities of between approximately 40 and 60 tons are anticipated for piles with a minimum shaft diameter of 4-inches. However, higher capacities are possible depending on the specific pile type/size proposed. The actual allowable capacity should be determined based upon the results of pile load testing conducted on the project site prior to final design. Also, the design of helical piles should consider the low lateral support provided by the shallow native soils and slenderness buckling should be evaluated for small diameter helical piles. In addition, where necessary, piles battered up to 15° should be utilized to carry lateral loads. A minimum 6-inch void form is recommended below grade beams..

7.2 Lateral Resistance for Seismic and Wind Loads

As discussed above, the native clay soils become softer with depth and are anticipated to provide limited lateral capacity for deep foundations. Based upon the results of the subsurface investigation, the following soil parameters are recommended for use in lateral pile capacity analyses:

Depth from Grade (in).	0 to 84	84+
Soil Type	Soft Clay	Soft Clay
Density (pci)	0.0637	0.0318
Cohesion (psi)	3	3
Friction Angle (ϕ)	0	0
ε ₅₀ (in/in)	0.02	0.02
K (pci)	200	200
$Modulus - K_h (tcf)$	15	15

In addition to lateral resistance of the piles, lateral resistance can be developed from sliding friction between the floor slab and the ground. In general, for the native soils, a sliding friction angle of 18° is recommended. This corresponds to a friction factor of 0.32.

7.3 Corrosion of Concrete and Steel

As discussed previously, the USDA Soil Survey Data indicates that the site soils have a high potential for corrosion of concrete. Therefore, at a minimum, Type I-II sulfate resistant cement is recommended for construction at this site.

The Soil Survey Data also indicates that the site soils have a high potential for corrosion of uncoated steel. Based upon our experience with similar soils in the vicinity of the project site, HBET believes that the native clay soils have a resistivity of less than 1,000 ohm-cm. The dense gravel soils are anticipated to have a resistivity of greater than 1,000 ohm-cm. Pile design should consider corrosion in their design based upon these resistivity values either through galvanization or accounting for section loss..



7.4 Non-Structural Floor Slabs and Exterior Flatwork

As mentioned above, expansive soils are present at the site. It is important to note that due to the fact that slabs-on-grade do not generate sufficient loads to resist heave, *differential movement of slabs-on-grade should be anticipated*. The only way to mitigate the risk of movement would be to use a structural floor slab supported by helical piles. However, this could be cost prohibitive. Although the risk of movement of a floating floor slab cannot be eliminated, the risk can be reduced by constructing a floating floor slab above a minimum of 30-inches of structural fill with subgrade preparation and fill placement in accordance with the *Spread Footings* section of this report. It is recommended that exterior slabs-on-grade be constructed above a minimum of 12-inches of structural fill.

Slabs-on-grade should not be tied into or otherwise connected to the foundations in any manner. In addition, interior, non-bearing partitions resting on the floor slab should include a framing void or slip joint which permits a minimum of 2-inches of vertical movement..

7.5 Lateral Earth Pressures

Stemwalls and/or retaining walls should be designed to resist lateral earth pressures. For backfill consisting of the native soils or imported granular, non-free draining, non-expansive material, we recommend that the walls be designed for an active equivalent fluid unit weight of 55 pcf in areas where no surcharge loads are present. An at-rest equivalent fluid unit weight of 75 pcf is recommended for braced walls. Lateral earth pressures should be increased as necessary to reflect any surcharge loading behind the walls.

7.6 Drainage

Due to the presence of moisture sensitive soils at the site, proper site grading is critical to the performance of the structure. In order to improve the long-term performance of the foundations and slabs-on-grade, grading around the structure should be designed to carry precipitation and runoff away from the structure. It is recommended that the finished ground surface drop at least twelve inches within the first ten feet away from the structure. However, where impermeable surfaces (i.e. pavements, sidewalks, etc.) are adjacent to the structure, the grade can be reduced to approximately 2.5-inches (ADA grade) within the first ten feet away from the structure.

HBET recommends that downspout extensions be used which discharge a minimum of 15 feet from the structure or beyond the backfill zone, whichever is greater. However, if subsurface downspout drains are utilized, they should be carefully constructed of solid-wall PVC and should daylight a minimum of 15 feet from the structure. In addition, an impermeable membrane is recommended below subsurface downspout drains. Dry wells should not be used.



In order to reduce the risk of surface moisture impacts to the structure, a perimeter foundation drain is recommended. In general, the perimeter foundation drain should consist of prefabricated drain materials or a perforated pipe and gravel system with the flowline of the drain at the bottom of the foundation (at the highest point). The perimeter drain should slope at a minimum of 1.0% to daylight or to a sump with pump. The drain should also include an impermeable membrane at the base to limit the potential for moisture to infiltrate vertically down below the foundation.

7.7 Excavations

Excavations in the soils at the site may stand for short periods of time but should not be considered to be stable. Trenching and excavations should be sloped back, shored, or shielded for worker protection in accordance with applicable OSHA standards. The soils generally classify as Type C soil with regard to OSHA's *Construction Standards for Excavations*. For Type C soils, the maximum allowable slope in temporary cuts is 1.5H:1V.

7.8 **Pavements**

The proposed construction may include paved automobile parking areas and truck traffic areas. As discussed previously, the pavement subgrade materials consist primarily of clay soils. As discussed previously, the native clay soils are moderately plastic and are anticipated to be slightly to moderately expansive. Therefore, the minimum recommended Resilient Modulus of 3,000 psi was used for the pavement design.

Based upon the subgrade conditions and anticipated traffic loading, flexible and rigid pavement section alternatives were developed in accordance with AASHTO design methodologies. The following minimum pavement section alternatives are recommended:

	PAVEMENT SECTION (Inches)								
ALTERNATIVE	Hot-Mix Asphalt Pavement	CDOT Class 6 Base Course	CDOT Class 3 Subbase Course	Concrete Pavement	TOTAL				
А	3.0	9.0			12.0				
В	4.0	7.0			11.0				
C	3.0	6.0	6.0		15.0				
Rigid Pavement		6.0		6.0	12.0				

Automobile Parking Areas EDL $\Lambda = 5$ Structural Number = 2

Truck Traffic Areas

EDLA = 20, Structural Number = 3.50

	PAVEMENT SECTION (Inches)									
ALTERNATIVE	Hot-Mix Asphalt Pavement	CDOT Class 3 CDOT Class 6 Base Course Course		Concrete Pavement	TOTAL					
А	3.0	15.0			18.0					
В	4.0	12.0			16.0					
С	3.0	6.0	13.0		22.0					
Rigid Pavement		6.0		8.0	14.0					



Prior to pavement placement, areas to be paved should be stripped of all topsoil, fill, or other unsuitable materials. It is recommended that the subgrade soils be scarified to a depth of 12-inches; moisture conditioned, and recompacted to a minimum of 95% of the standard Proctor maximum dry density, within $\pm 2\%$ of optimum moisture content as determined by AASHTO T-99.

Aggregate base course and subbase course should be placed in maximum 9-inch loose lifts, moisture conditioned, and compacted to a minimum of 95% and 93% of the maximum dry density, respectively, at -2% to +3% of optimum moisture content as determined by AASHTO T-180. In addition to density testing, base course should be proofrolled to verify subgrade stability.

It is recommended that Hot-Mix Asphaltic (HMA) pavement conform to CDOT grading SX or S specifications and consist of an approved 75 gyration Superpave method mix design. HMA pavement should be compacted to between 92% and 96% of the maximum theoretical density. An end point stress of 50 psi should be used. It is recommended that rigid pavements consist of CDOT Class P concrete or alternative approved by the Engineer. In addition, pavements should conform to local specifications.

The long-term performance of the pavements is dependent on positive drainage away from the pavements. Ditches, culverts, and inlet structures in the vicinity of paved areas must be maintained to prevent ponding of water on the pavement.

8.0 GENERAL

The recommendations included above are based upon the results of the subsurface investigation and on our local experience. These conclusions and recommendations are valid only for the proposed construction.

As discussed previously, the subsurface conditions encountered in the borings were slightly variable. However, the precise nature and extent of any subsurface variability may not become evident until construction. As a result, it is recommended that HBET provide construction materials testing and engineering oversight during the entire construction process.

It is important to note that the recommendations herein are intended to reduce the risk of structural movement and/or damage, to varying degrees, associated with volume change of the native soils. However, HBET cannot predict long-term changes in subsurface moisture conditions and/or the precise magnitude or extent of volume change. Where significant increases in subsurface moisture occur due to poor grading, improper stormwater management, utility line failure, excess irrigation, or other cause, either during construction or the result of actions of the property owner, several inches of movement are possible. In addition, any failure to comply with the recommendations in this report releases Huddleston-Berry Engineering & Testing, LLC of any liability with regard to the structure performance.



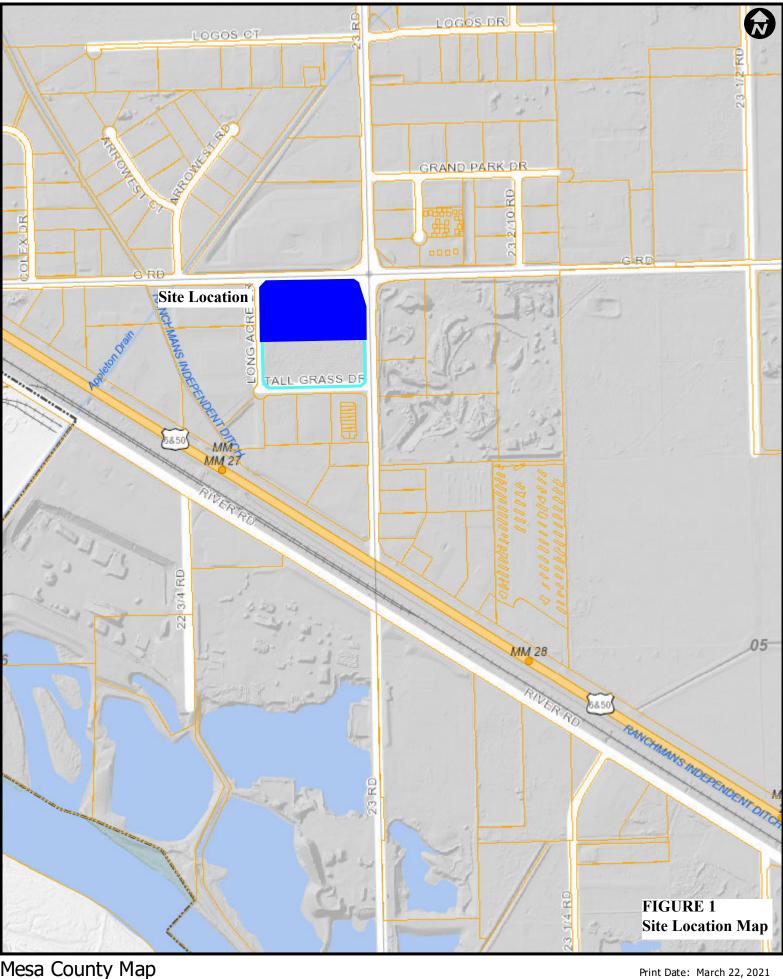
Huddleston-Berry Engineering and Testing, LLC is pleased to be of service to your project. Please contact us if you have any questions or comments regarding the contents of this report.

Respectfully Submitted: Huddleston-Berry Engineering and Testing, LLC



Michael A. Berry, P.E. Vice President of Engineering

FIGURES



Mesa County Map

						Time Duce
The Geographic Information System (GIS) and its components are designed as a source of reference for answering inquiries, for planning and for modeling GIS is not intended or does not replace legal description information in the chain of title and	0	0.05	0.1	0.2 mi	\frown	
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the representations of location in this GIS cannot be substitute for actual legal surveys. The information contained herein is believed accurate and suitable for the limited uses, and subject to the limitations, set forth		0.075	0 1 5	0.2 km		GIS/IT
above. Mesa County makes no warranty as to the accuracy or suitability of any information contained herein. Users assume al Irisk and responsibility for any and al damages, including consequential damages, which may flow from the user's use of this information.	0	0.075	0.15	0.3 km		ais r

ounty, Colorado IT Department gis.mes



Print Date: March 22, 2021 0.06 mi Mesa County, Colorado **GIS/IT Department**

Messa County Map The Gographic Information System (GIS) and its components are designed as a source of reference for answering inquiries, for planning and for modeling GIS is not interded or does not replace legal description information in the dain of title and their information contained in d'ficial government records such as the County Clerk and Recorders office or the carts. In addition, the representations of location in this GIS cannot be substrute for adrual legal survey. The information contained herein is believed accuster and suibble for the limited uses, and subject to the limitations, set forth source, Marsa County makes now variarity as to the accuracy or suitability of any information contained herein. Users assume alirisk and responsibility for any and aldamages, including consequential damages, which may flow from the user's use of this information. 0.0175 0.035 0

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0.07 km

0.03

APPENDIX A Soil Survey Data



Web Soil Survey National Cooperative Soil Survey

MA	P LEGEND		MAP INFORMATION		
Area of Interest (AOI)	Spo	il Area	The soil surveys that comprise your AOI were mapped at		
Area of Interest (A		ny Spot	1:24,000.		
Soils	m Very	y Stony Spot	Warning: Soil Map may not be valid at this scale.		
Soil Map Unit Poly	jons	t Spot	Enlargement of maps beyond the scale of mapping can cause		
Soil Map Unit Lines	∆ Othe		misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of		
Soil Map Unit Poin	s 🗳	cial Line Features	contrasting soils that could have been shown at a more detailed		
Special Point Features	Water Features		scale.		
Blowout		eams and Canals	Please rely on the bar scale on each map sheet for map		
Borrow Pit	Transportation		measurements.		
💥 Clay Spot	++++ Rail	s	Source of Map: Natural Resources Conservation Service		
Closed Depression	🛹 Inter	rstate Highways	Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)		
💥 Gravel Pit	JUS I	Routes	Maps from the Web Soil Survey are based on the Web Mercate		
Gravelly Spot	🥪 Majo	or Roads	projection, which preserves direction and shape but distorts		
🔕 Landfill	Loca	al Roads	distance and area. A projection that preserves area, such as th Albers equal-area conic projection, should be used if more		
Lava Flow	Background		accurate calculations of distance or area are required.		
Marsh or swamp	•	ial Photography	This product is generated from the USDA-NRCS certified data of the version date(s) listed below.		
Mine or Quarry					
Miscellaneous Wat	er		Soil Survey Area: Mesa County Area, Colorado Survey Area Data: Version 11, Jun 8, 2020		
O Perennial Water			Soil map units are labeled (as space allows) for map scales		
Rock Outcrop			1:50,000 or larger.		
Saline Spot			Date(s) aerial images were photographed: Sep 13, 2010—Au 8, 2017		
Sandy Spot					
Severely Eroded S	oot		The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background		
Sinkhole			imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.		
Slide or Slip			Sinting of map this boundaries may be evident.		
🦻 Sodic Spot					
yg cours open					



Map Unit Legend

Map Unit Symbol Map Unit Name		Acres in AOI	Percent of AOI
BaS	Massadona silty clay loam, saline surface, 0 to 2 percent slopes	12.5	100.0%
Totals for Area of Interest		12.5	100.0%



Map Unit Description

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions in this report, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named, soils that are similar to the named components, and some minor components that differ in use and management from the major soils.

Most of the soils similar to the major components have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Some minor components, however, have properties and behavior characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities. Soils that have profiles that are almost alike make up a *soil series*. All the soils of a series have major horizons that are similar in composition, thickness, and arrangement. Soils of a given series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Additional information about the map units described in this report is available in other soil reports, which give properties of the soils and the limitations, capabilities, and potentials for many uses. Also, the narratives that accompany the soil reports define some of the properties included in the map unit descriptions.

Report—Map Unit Description

Mesa County Area, Colorado

BaS—Massadona silty clay loam, saline surface, 0 to 2 percent slopes

Map Unit Setting National map unit symbol: k06p

USDA

Elevation: 4,490 to 4,920 feet *Mean annual precipitation:* 6 to 9 inches *Mean annual air temperature:* 50 to 55 degrees F *Frost-free period:* 140 to 180 days *Farmland classification:* Not prime farmland

Map Unit Composition

Massadona, saline surface, and similar soils: 70 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Massadona, Saline Surface

Setting

Landform: Fan remnants Down-slope shape: Linear Across-slope shape: Linear Parent material: Cretaceous source alluvium derived from clayey shale

Typical profile

Apz - 0 to 2 inches: silty clay loam Bwz - 2 to 12 inches: silty clay Bkyz - 12 to 24 inches: silty clay BCkyz1 - 24 to 48 inches: fine sandy loam BCkyz2 - 48 to 60 inches: silty clay loam

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.07 to 0.21 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 15 percent
Gypsum, maximum content: 2 percent
Maximum salinity: Strongly saline (16.0 to 40.0 mmhos/cm)
Available water capacity: Low (about 4.7 inches)

Interpretive groups

Land capability classification (irrigated): 7s Land capability classification (nonirrigated): 7c Hydrologic Soil Group: C Ecological site: R034BY103UT - Desert Clay (Castlevalley saltbush) Hydric soil rating: No

Data Source Information

Soil Survey Area: Mesa County Area, Colorado Survey Area Data: Version 11, Jun 8, 2020

Dwellings and Small Commercial Buildings

Soil properties influence the development of building sites, including the selection of the site, the design of the structure, construction, performance after construction, and maintenance. This table shows the degree and kind of soil limitations that affect dwellings and small commercial buildings.

The ratings in the table are both verbal and numerical. Rating class terms indicate the extent to which the soils are limited by all of the soil features that affect building site development. *Not limited* indicates that the soil has features that are very favorable for the specified use. Good performance and very low maintenance can be expected. *Somewhat limited* indicates that the soil has features that are moderately favorable for the specified use. The limitations can be overcome or minimized by special planning, design, or installation. Fair performance and moderate maintenance can be expected. *Very limited* indicates that the soil has one or more features that are unfavorable for the specified use. The limitations can be overcome without major soil reclamation, special design, or expensive installation procedures. Poor performance and high maintenance can be expected.

Numerical ratings in the table indicate the severity of individual limitations. The ratings are shown as decimal fractions ranging from 0.01 to 1.00. They indicate gradations between the point at which a soil feature has the greatest negative impact on the use (1.00) and the point at which the soil feature is not a limitation (0.00).

Dwellings are single-family houses of three stories or less. For dwellings without basements, the foundation is assumed to consist of spread footings of reinforced concrete built on undisturbed soil at a depth of 2 feet or at the depth of maximum frost penetration, whichever is deeper. For dwellings with basements, the foundation is assumed to consist of spread footings of reinforced concrete built on undisturbed soil at a depth of about 7 feet. The ratings for dwellings are based on the soil properties that affect the capacity of the soil to support a load without movement and on the properties that affect excavation and construction costs. The properties that affect the load-supporting capacity include depth to a water table, ponding, flooding, subsidence, linear extensibility (shrink-swell potential), and compressibility. Compressibility is inferred from the Unified classification. The properties that affect the ease and amount of excavation include depth to a water table, ponding, flooding, slope, depth to bedrock or a cemented pan, hardness of bedrock or a cemented pan, and the amount and size of rock fragments.

Small commercial buildings are structures that are less than three stories high and do not have basements. The foundation is assumed to consist of spread footings of reinforced concrete built on undisturbed soil at a depth of 2 feet or at the depth of maximum frost penetration, whichever is deeper. The ratings are based on the soil properties that affect the capacity of the soil to support a load without movement and on the properties that affect excavation and construction costs. The properties that affect the load-supporting capacity include depth to a water table, ponding, flooding, subsidence, linear extensibility (shrink-swell potential), and compressibility (which is inferred from the Unified classification). The properties that affect the ease and amount of excavation include flooding, depth to a water table, ponding, slope, depth to bedrock or a cemented pan, hardness of bedrock or a cemented pan, and the amount and size of rock fragments.

Information in this table is intended for land use planning, for evaluating land use alternatives, and for planning site investigations prior to design and construction. The information, however, has limitations. For example, estimates and other data generally apply only to that part of the soil between the surface and a depth of 5 to 7 feet. Because of the map scale, small areas of different soils may be included within the mapped areas of a specific soil.

The information is not site specific and does not eliminate the need for onsite investigation of the soils or for testing and analysis by personnel experienced in the design and construction of engineering works.

Government ordinances and regulations that restrict certain land uses or impose specific design criteria were not considered in preparing the information in this table. Local ordinances and regulations should be considered in planning, in site selection, and in design.

Report—Dwellings and Small Commercial Buildings

[Onsite investigation may be needed to validate the interpretations in this table and to confirm the identity of the soil on a given site. The numbers in the value columns range from 0.01 to 1.00. The larger the value, the greater the potential limitation. The table shows only the top five limitations for any given soil. The soil may have additional limitations]

	Dwellings and Small Commercial Buildings–Mesa County Area, Colorado											
Map symbol and soil name	Pct. of map	Dwellings without basements		Dwellings with base	ements	Small commercial buildings						
	unit	Rating class and limiting features	Value	Rating class and limiting features	Value	Rating class and limiting features	Value					
BaS—Massadona silty clay loam, saline surface, 0 to 2 percent slopes												
Massadona, saline surface	70	Somewhat limited		Somewhat limited		Somewhat limited						
		Shrink-swell	0.17	Shrink-swell	0.06	Shrink-swell	0.17					

Data Source Information

Soil Survey Area: Mesa County Area, Colorado Survey Area Data: Version 11, Jun 8, 2020



Roads and Streets, Shallow Excavations, and Lawns and Landscaping

Soil properties influence the development of building sites, including the selection of the site, the design of the structure, construction, performance after construction, and maintenance. This table shows the degree and kind of soil limitations that affect local roads and streets, shallow excavations, and lawns and landscaping.

The ratings in the table are both verbal and numerical. Rating class terms indicate the extent to which the soils are limited by all of the soil features that affect building site development. *Not limited* indicates that the soil has features that are very favorable for the specified use. Good performance and very low maintenance can be expected. *Somewhat limited* indicates that the soil has features that are moderately favorable for the specified use. The limitations can be overcome or minimized by special planning, design, or installation. Fair performance and moderate maintenance can be expected. *Very limited* indicates that the soil has one or more features that are unfavorable for the specified use. The limitations generally cannot be overcome without major soil reclamation, special design, or expensive installation procedures. Poor performance and high maintenance can be expected.

Numerical ratings in the table indicate the severity of individual limitations. The ratings are shown as decimal fractions ranging from 0.01 to 1.00. They indicate gradations between the point at which a soil feature has the greatest negative impact on the use (1.00) and the point at which the soil feature is not a limitation (0.00).

Local roads and streets have an all-weather surface and carry automobile and light truck traffic all year. They have a subgrade of cut or fill soil material; a base of gravel, crushed rock, or soil material stabilized by lime or cement; and a surface of flexible material (asphalt), rigid material (concrete), or gravel with a binder. The ratings are based on the soil properties that affect the ease of excavation and grading and the traffic-supporting capacity. The properties that affect the ease of excavation and grading are depth to bedrock or a cemented pan, hardness of bedrock or a cemented pan, depth to a water table, ponding, flooding, the amount of large stones, and slope. The properties that affect the traffic-supporting capacity are soil strength (as inferred from the AASHTO group index number), subsidence, linear extensibility (shrink-swell potential), the potential for frost action, depth to a water table, and ponding.

Shallow excavations are trenches or holes dug to a maximum depth of 5 or 6 feet for graves, utility lines, open ditches, or other purposes. The ratings are based on the soil properties that influence the ease of digging and the resistance to sloughing. Depth to bedrock or a cemented pan, hardness of bedrock or a cemented pan, the amount of large stones, and dense layers influence the ease of digging, filling, and compacting. Depth to the seasonal high water table, flooding, and ponding may restrict the period when excavations can be made. Slope influences the ease of using machinery. Soil texture, depth to the water table, and linear extensibility (shrink-swell potential) influence the resistance to sloughing.

Lawns and landscaping require soils on which turf and ornamental trees and shrubs can be established and maintained. Irrigation is not considered in the ratings. The ratings are based on the soil properties that affect plant growth and trafficability after vegetation is established. The properties that affect plant growth are reaction; depth to a water table; ponding; depth to bedrock or a cemented pan; the available water capacity in the upper 40 inches; the content of salts, sodium, or calcium carbonate; and sulfidic materials. The properties that affect trafficability are flooding, depth to a water table, ponding, slope, stoniness, and the amount of sand, clay, or organic matter in the surface layer.

Information in this table is intended for land use planning, for evaluating land use alternatives, and for planning site investigations prior to design and construction. The information, however, has limitations. For example, estimates and other data generally apply only to that part of the soil between the surface and a depth of 5 to 7 feet. Because of the map scale, small areas of different soils may be included within the mapped areas of a specific soil.

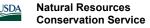
The information is not site specific and does not eliminate the need for onsite investigation of the soils or for testing and analysis by personnel experienced in the design and construction of engineering works.

Government ordinances and regulations that restrict certain land uses or impose specific design criteria were not considered in preparing the information in this table. Local ordinances and regulations should be considered in planning, in site selection, and in design.

Report—Roads and Streets, Shallow Excavations, and Lawns and Landscaping

[Onsite investigation may be needed to validate the interpretations in this table and to confirm the identity of the soil on a given site. The numbers in the value columns range from 0.01 to 1.00. The larger the value, the greater the potential limitation. The table shows only the top five limitations for any given soil. The soil may have additional limitations]

Roads and	Roads and Streets, Shallow Excavations, and Lawns and Landscaping–Mesa County Area, Colorado											
Map symbol and soil	Pct. of	Lawns and landsca	aping	Local roads and st	reets	Shallow excavati	Shallow excavations					
name	map unit	Rating class and limiting features	Value	Rating class and limiting features	Value	Rating class and limiting features	Value					
BaS—Massadona silty clay loam, saline surface, 0 to 2 percent slopes												
Massadona, saline surface	70	Very limited		Very limited		Somewhat limited						
		Salinity	1.00	Low strength	1.00	Dusty	0.50					
		Dusty	0.50	Shrink-swell	0.17	Too clayey	0.02					
		Droughty	0.11			Unstable excavation walls	0.01					



Data Source Information

Soil Survey Area: Mesa County Area, Colorado Survey Area Data: Version 11, Jun 8, 2020



Soil Features

This table gives estimates of various soil features. The estimates are used in land use planning that involves engineering considerations.

A *restrictive layer* is a nearly continuous layer that has one or more physical, chemical, or thermal properties that significantly impede the movement of water and air through the soil or that restrict roots or otherwise provide an unfavorable root environment. Examples are bedrock, cemented layers, dense layers, and frozen layers. The table indicates the hardness and thickness of the restrictive layer, both of which significantly affect the ease of excavation. *Depth to top* is the vertical distance from the soil surface to the upper boundary of the restrictive layer.

Subsidence is the settlement of organic soils or of saturated mineral soils of very low density. Subsidence generally results from either desiccation and shrinkage, or oxidation of organic material, or both, following drainage. Subsidence takes place gradually, usually over a period of several years. The table shows the expected initial subsidence, which usually is a result of drainage, and total subsidence, which results from a combination of factors.

Potential for frost action is the likelihood of upward or lateral expansion of the soil caused by the formation of segregated ice lenses (frost heave) and the subsequent collapse of the soil and loss of strength on thawing. Frost action occurs when moisture moves into the freezing zone of the soil. Temperature, texture, density, saturated hydraulic conductivity (Ksat), content of organic matter, and depth to the water table are the most important factors considered in evaluating the potential for frost action. It is assumed that the soil is not insulated by vegetation or snow and is not artificially drained. Silty and highly structured, clayey soils that have a high water table in winter are the most susceptible to frost action. Well drained, very gravelly, or very sandy soils are the least susceptible. Frost heave and low soil strength during thawing cause damage to pavements and other rigid structures.

Risk of corrosion pertains to potential soil-induced electrochemical or chemical action that corrodes or weakens uncoated steel or concrete. The rate of corrosion of uncoated steel is related to such factors as soil moisture, particle-size distribution, acidity, and electrical conductivity of the soil. The rate of corrosion of concrete is based mainly on the sulfate and sodium content, texture, moisture content, and acidity of the soil. Special site examination and design may be needed if the combination of factors results in a severe hazard of corrosion. The steel or concrete in installations that intersect soil boundaries or soil layers is more susceptible to corrosion than the steel or concrete in installations that are entirely within one kind of soil or within one soil layer.

For uncoated steel, the risk of corrosion, expressed as *low*, *moderate*, or *high*, is based on soil drainage class, total acidity, electrical resistivity near field capacity, and electrical conductivity of the saturation extract.

For concrete, the risk of corrosion also is expressed as *low, moderate*, or *high.* It is based on soil texture, acidity, and amount of sulfates in the saturation extract.

Report—Soil Features

	Soil Features–Mesa County Area, Colorado											
Map symbol and		Res	strictive Layer		Subsidence		Potential for frost	Risk of d	corrosion			
soil name —	Kind	Depth to top	Thickness	Hardness	Initial	Total	- action	Uncoated steel	Concrete			
		Low-RV- High	Range		Low- High	Low- High						
		In	In		In	In						
BaS—Massadona silty clay loam, saline surface, 0 to 2 percent slopes												
Massadona, saline surface		-			0	0	Low	High	High			

Data Source Information

Soil Survey Area: Mesa County Area, Colorado Survey Area Data: Version 11, Jun 8, 2020



APPENDIX B Typed Boring Logs

Engeneration of the second	B B CONSUL	Huddleston-Berry Engineering & Testing, LLC 2789 Riverside Parkway Grand Junction, CO 81501 970-255-8005					BO	RIN	IGN	IUN		R E E 1 C	
CLIE	NT Fo	od Bank of the Rockies	PROJECT	NAME	2294	Tall Grass	Drive						
			PROJECT										
		TED <u>3/10/21</u> COMPLETED <u>3/10/21</u>							SIZE	4-Inc	ch		
		ONTRACTOR S. McKracken											
		IETHOD Simco 2000 Track Rig				LING) ft						
		CHECKED BY MAB	_			.ING 13.0							
										ATI	ERBE	ERG	F
o DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID		s \	FINES CONTENT (%)
0	<u>71 1×</u> .71	Sandy Clay with Organics (TOPSOIL)											
	11. 11,												
		Lean CLAY (CL), brown to gray to reddish-brown, moist to soft to very stiff	o wet,										
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20	<i>\\\\\</i>		Ľ	4	95	3-5-6/0"	4						
		Bottom of hole at 20.5 feet.											

Engle	B B CONSUL	Huddleston-Berry Engineering & Testing, LLC 2789 Riverside Parkway Grand Junction, CO 81501 970-255-8005					BO	RIN	IG N	IUN	IBE PAGE		
CLIE	NT Fo	od Bank of the Rockies	PROJEC	T NAME	2294	Tall Grass	Drive						
PRO.	IECT N	UMBER 01282-0002	_ PROJEC	T LOCAT		Grand June	ction, (0					
		TED 3/10/21 COMPLETED 3/10/21						HOLE	SIZE				
DRIL	LING C	ONTRACTOR S. McKracken											
DRIL		ETHOD Simco 2000 Track Rig				LING 9.0							
LOGO	GED B	SD CHECKED BY MAB	_ ¥ at	END OF	DRILL	ING <u>9.0 f</u>	t						
NOTE	S		_ AF	TER DRI	LLING								
o DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID LIMIT		3	FINES CONTENT (%)
	<u>7, 1</u> 7. 77	Sandy Clay with Organics (TOPSOIL)											
		Lean CLAY (cl), brown, moist to wet, soft to very stiff		V ss	44	4-8-11	-						
				1	44	(19)	-						
				SS 2	61	4-7-9 (16)	-						
 - 10		Y .											
				ss 3	0	1-2-0 (2)	-						
20		Sandy GRAVELS (gp-gc), brown, wet, very dense											
20 20	•	Bottom of hole at 20.5 feet.		SS 4	100	30/5"							

		Huddleston-Berry Engineering & Testing, LLC 2789 Riverside Parkway Grand Junction, CO 81501 970-255-8005					BO	RIN	IG N	IUN		R B ≣ 1 0	
CLIEN	IT Foo	od Bank of the Rockies	PROJECT N	IAME	2294	Tall Grass	Drive						
		JMBER 01282-0002	PROJECT L										
		ED _3/10/21 COMPLETED _3/10/21							SIZE				
		DNTRACTOR S. McKracken											
		ETHOD Simco 2000 Track Rig				LING 7.0	ft						
		SD CHECKED BY MAB				.ING 7.0 f							
							-						
									1	ΔΤΊ	ERBE	RG	
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION	Somer E TVDE	SAMPLE I YFE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIMIT		3	FINES CONTENT (%)
0	<u>x 1/2</u> <u>x 1</u>	Sandy Clay with Organics (TOPSOIL)										<u> </u>	-
	1/ 1/												
		Lean CLAY (cl), brown, moist to wet, very soft to very stiff											
· _													
			X	SS 1	78	8-10-10				41	21	20	
· _			$\langle \rangle$			(20)							
5													
· _													
		-											
_		<u>.</u>											
			X	SS 2	83	9-10-15							
-			$\langle \rangle$	2		(25)							
_													
10													
-													
-													
			X	SS 3	28	1-1-0 (1)							
-			\square	5		(1)							
				_									
15													
-													
_													
_		Sandy GRAVELS (gp-gc), brown, wet, dense											
20	o YZ												
	0	Bottom of hole at 20.5 feet.											

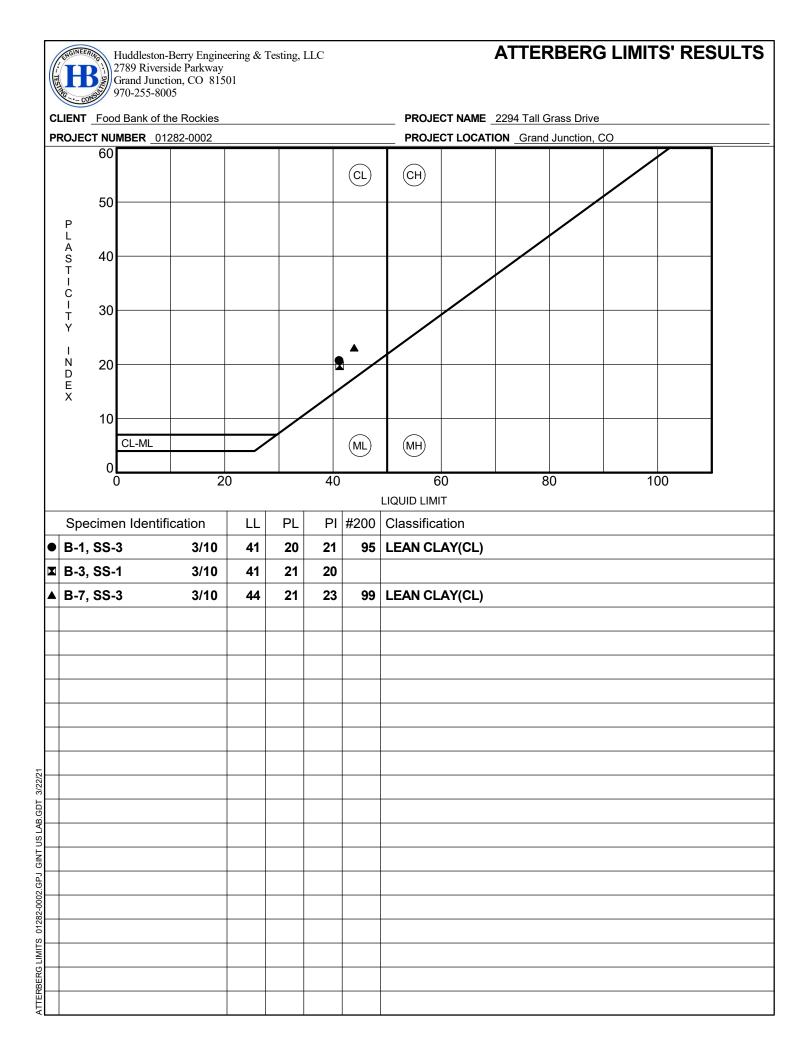
Entre I	B B COMBIN	Huddleston-Berry Engineering & Testing, LLC 2789 Riverside Parkway Grand Junction, CO 81501 970-255-8005					BO	RIN	IG N	IUN	IBE PAGE		
CLIE	NT Fo	od Bank of the Rockies	PROJEC	T NAME	2294	Tall Grass	Drive						
		UMBER 01282-0002				Grand Jun							
		TED 3/10/21 COMPLETED 3/10/21						HOLE	SIZE				
		ONTRACTOR S. McKracken					с						
		ETHOD Simco 2000 Track Rig (SD CHECKED BY MAB	_			LING <u>8.0</u> LING 8.0 f							
				TER DRI									
									_	ATT	ERBE	RG	F
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID		~	FINES CONTENT (%)
0	<u> </u>	Sandy Clay with Organics (TOPSOIL)											
- ·		Lean CLAY (cl), brown, moist to wet, soft to hard											
- ·				∬ ss		7-8-9	-						
					56	(17)							
5													
L .													
		-		V ss	72	11-16-21							
		<u>v</u>		2		(37)	-						
10													
- ·							-						
ļ .					0	0-1-1 (2)							
				<u>/</u>									
15													
- ·													
20		Sandy GRAVELS (gp-gc), brown, wet, very dense		ss 4	50	1-5-16-21							
				4	30	(21)							
		Bottom of hole at 21.0 feet.					1						
j													

- TESTING	R	Huddleston-Berry Engineering & Testing, LLC 2789 Riverside Parkway Grand Junction, CO 81501 970-255-8005					BO	RIN	IG N	IUN		R E E 1 C	
CLIEN	T For	od Bank of the Rockies	PROJEC		2294	Tall Grass	Drive	l					
PROJI	ECT NU	JMBER _01282-0002	PROJEC			Grand Jun	ction,	со					
		ED _3/10/21 COMPLETED _3/10/21						HOLE	SIZE				
		ONTRACTOR S. McKracken											
		ETHOD Simco 2000 Track Rig				LING <u>9.0</u>							
		SD CHECKED BY MAB				.ING 9.0 f							
NOTE	s		_ AF	IER DRI			1			A T 1	ERBE		
	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)			s ≻	FINES CONTENT
0.0	<u>x¹ 1_x x¹</u>	Sandy Clay with Organics (TOPSOIL)										-	
-													
_		Lean CLAY (cl), brown, moist to wet, soft to very stiff											
_		Lean OLAT (07, BIOWN, MOISE to Wet, Soit to Very Still											1
2.5													
2.3				∛ ss	67	11-11-11							
_				1	07	(22)							
_				/ \									
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5.0													
-													
-													
7.5				$\backslash /$									
				∦ ss 2	72	4-4-7 (11)							
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				∦ SS ∦ 3	28	2-1-1 (2)							
-				/ \									
ļ		Bottom of hole at 11.5 feet.		<u> </u>			1						

TESTING	IGINEER	:	Huddleston-Berry Engineering & Testing, LLC 2789 Riverside Parkway Grand Junction, CO 81501 970-255-8005					BO	RIN	IG N	NUN	IBE PAGE	
CLI	ENT	Fo	od Bank of the Rockies	PROJEC	T NAME	2294	Tall Grass	Drive					
PR	OJEC						Grand June						
DA	TE ST	AR	COMPLETED	GROUND) ELEVA				HOLE	SIZE			
DRI	LLING	G CO	DNTRACTOR S. McKracken	GROUN	WATER		LS:						
DR	LLING	g Mi	ETHOD Simco 2000 Track Rig	$ar{ abla}$ at	TIME OF	DRIL	LING _10.0) ft					
LO	GGED) BY	SD CHECKED BY MAB	▼ AT	END OF	DRILL	.ING <u>10.0</u>	ft					
NO	TES			AF	ter dri	LLING							
o DEPTH		FOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIMIT LIMIT		FINES CONTENT (%)
		<u></u>	Sandy Clay with Organics (TOPSOIL)										
- - - - - - - - - - - - - - - - - - -			Sandy Clay with Organics (TOPSOIL)		SS 1	67	8-10-17 (27) 6-12-14 (26)						
1 3/23/2					SS 3	0	1-0-0 (0)						
AB.GL					<u>v N</u>								
15													
01282-0002.6P3													
SNIMO	60		Sandy GRAVELS (gp-gc), brown, wet, very dense										
			Bottom of hole at 18.5 feet.		SS 4	100	30/3"						

TESTING !!	B	Huddleston-Berry Engineering & Testing, LLC 2789 Riverside Parkway Grand Junction, CO 81501 970-255-8005					BO	RIN	IG N	IUN		R E = 1 C	
CLIE	NT Foo	d Bank of the Rockies	PROJEC	T NAME	2294	Tall Grass	Drive	!					
		MBER 01282-0002											
		ED 3/10/21 COMPLETED 3/10/21						HOLE	SIZE				
		NTRACTOR Simon 2000 Track Dir											
		Simco 2000 Track Rig SD CHECKED BYMAB				LING <u>dry</u> .ING <u>dry</u>							
					%			-	()	ATT	ERBE		NT
DEPTH (ft)	GRAPHIC LOG	MATERIAL DESCRIPTION		SAMPLE TYPE NUMBER	RECOVERY ((RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (tsf)	DRY UNIT WT. (pcf)	MOISTURE CONTENT (%)	LIQUID			FINES CONTENT
0.0	<u>x1 1, x1</u>	Sandy Clay with Organics (TOPSOIL)										<u>a</u>	ш
-	1/ 1//												
-		Lean CLAY (CL), brown, moist , medium stiff to very stiff											
- 2.5				ss 1	67	11-11-14 (25)	-						
-				/ \			-						
5.0													
-													
-													
<u>7.5</u>				ss 2	89	9-12-16 (28)							
-													
<u>10.0</u>		**Lab Classified SS-3				2-3-3	_						
-				SS 3	50	(6)				44	21	23	9
-		Bottom of hole at 11.5 feet.		<u> </u>									

APPENDIX C Laboratory Testing Results



IESIN	NGINEERING HB	2789 Grand	lleston-E Riversio d Junctio 255-800:	de Pa on, C	rkwav	7	ıg &	Testii	ng, I	LLC	2											C	SR	R A	IN	SIZ	ZE	C	DIS	ST	RI	BU [.]	TIC	NC
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×	B-7, S	S-3	3/1	0		4.75	5														0	.0			_1	1.0					9	9.0		
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